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TITLE: EUTECTIC COMPOSITE EXPLOSIVES CONTAINING AMMONIUM NITRATE

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MASTER

SUBMITTED TO: 7th Symposium (Intl) on Detonation Annapolis, MD

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EUTECTIC COMPOSITE EXPLOSIVES CONTAINING AMMONIUM NITRATE

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We have prepared, and studied the sensitivity and performance of, the eutectic of ammonium nitrate (AN) and the ammonium salt of 3,5-dinitro-1,2,4-triazole. We found that this AN formulation was unusual in that it performed ideally at small diameter, which indicated that it was a monomolecular explosive. Sensitivity tests included type 12 impact, Henkin thermal and wedge tests, and performance tests included rate stick/plate dent, cylinder, and aquarium tests. Pesults were compared with calculations, standard explosives, and another eutectic, ethylenedismine dinitrate (EDD)/AN.

I. INTRODUCTION

Monomplecular explosives are. limited in amount of energy that can he built into the molecule without it becoming too unstable to use. However, if all the oxygen does not have to be in the same molecule, a more stable combination of oxidizer and fuel-rich explosive can achieve the energy of a CO2-balanced explosive. Until recently, it had been thought (1) that a solid solution would be necessary for an exidizer and fuel to behave as one compound in the detonation zone. However, experiments by Finger (2) and co-workers at Lawrence Livermore National Laboratory (LLNL) showed that when the particle size of the oxidizer was less than 5 um (for example, a composite of ground particles of ammonium perchlorate suspended in yelled nitromethane) then the oxidizer reacts completely in the detonation zone, as shown by the scaling be-tween 2.54- and 5.08-cm-diam cylinder tests. McGuire (3) found that isotopic mixing during detonation in a monomolecular explosive was random. But in the case of a composite, Anatol (N¹)-labeled asmonium nitrate (AN)/-TNT) the isotope ratio in the products indicated that only a 0.6 .m layer of the AN particles combined with the

atoms of TNT in the detonation zone before the products were frozen out (3). These two experiments show that if the particle size of the oxidizer is less than about 1 m, a solid solution will not be necessary to get complete reaction in the detonation zone.

Akst and Hershkowitz found that cosolidification of AN with other amine mitrates increased the participation of AN in the defination. They found the eutentic of AN with ethylenediamine dinitrate (EDD) especially interesting because its melting point at 103°C would make it a useful dasting matrix (4,5,5). They found some is rovement in the amount of AN reacting in the detonation zone, but their experiments with FED/AN at Picatinny Argenal (now 0.5. Army Armanment Research and Development Command. ARRADCOM) were limited to small diameter detonation velocities (D). did not come close to raidulated values of D at these diameters.

At the name time at Los Alamou National Laboratory, we began to study the extection of AN with the assonium salts of nitroheterocycles. One of these, the extectio of AN with the assonium salt of 3,5-dinitro-1,2,4-triazoly (ADNT) was stable as a melt from 112 to 130°C, and needed only

two moles of AN per mole of ADNT to be CO₂-balanced. Because the CO₂-formulation was not far from eutectic formulation, 1.38/1 molar ratio AN/-ADNT, all of the AN could be dissolved in the eutectic melt by heating to 123°C (7). We have studied the performance of the eutectic and 2/1 molar ratio AN/ADNT, compared these results with calculated results and compared our results with those Akst has obtained for eutectic EDD/AN (8).

II. MATERIAL FREPARATION

Preparation of ADNT

We have modified the method of preparation of ADNT reported by the Soviets (9), especially the method of isolation. The following is a sample synthesis and isolation.

A solution of 3,5-diamino-1,2,4,- triazole (Aldrich) (30.0 g. 0.3 mol) in 0.68 M sulfuric acid (1.1 /, 1.5 mol H+) was added dropwise over 3 hours to a solution of sodium nitrite (200 g, 2.9 mol) in water (200 ml) while keeping the reaction mixture at 0°C with an alcohol-ic bath. After addition was complete, the re-action was heated to 60°C and was held there for one hour until all precipitate had dissolved. Then the reaction mixture was cooled again to $0^{\circ}C$, and acidified with 6 M sulfuric acid (100 ml, 1.2 mol H $^{+}$). This step converted the excess rodium nitrite to nitrous acid. Urea (15 g, 0.25 mol) was added slowly (foaming) to remove any remaining oxides of nitrogen from solution. The completed reaction mixture had a small amount of orange precipitate that was removed by addition of decolorizing carbon and filtration. Analysis of the filtrate by ultraviolet spectroscopy at 285 nm snowed a 90% yield of 3,5-dinitro-1,2,4-triazole (DNT).

The strongly acidic character of DNT (-0.66 pRs) (10) made extraction with the usual organic solvents impossible. It can be extracted by the continuous method with ethyl ether, but the flammability of ether made another method necessary for large-scale reactions. We found that a toluere solution (20%) of water-insoluble secondary or tertiary amines extracted the DNT from the aqueous reaction mixture (11). Ammonia gas bubbled into the dried organic phase regenerated the amine and precipitated the desired ammonium salt, ADNT. Recrystallization in 90/10 volume ratio ethyl acetate/acetone and drying over

Drierite in vacuum gave pure ADNT (35 g, 0.2 mol, 67% yield) with a melting point of 168-170°C. The yield was improved by a second extraction of the aqueous reaction mixture. ADNT forms a dihydrate at relative humidities over 35%. The amines used were tertiary amines: Alamines 304 and 336 (General Mill Chemicals, Inc.) and a secondary amine: Amberlite (Rohm and Haas Co.). The molar amount of amine used was equal to the amount of the DNT in the solution as measured by uv spectroscopy. The regenerated amine solution was reused after washing with water.

Preparation of Amine Nitrates

We prepared EDD and other aliphatic amine nitrates by dissolving the amine in 10% aqueous methanol and adding 10/50 by volume concentrated nitric acid/water dropwise while cooling with an ice bath to keep the temperature at ambient or below. After neutralization was complete, the pre-injutated nitrate salt was filtered, washed well with methanol, and recrystallized from water/methanol.

Preparation of AN/ADNT Mixes

Dry AN and ADNT (overnight in a vacuum desiccator over Drierite) were mixed and melted in a beaker heated by a heating bath or a heating block with a temperature between 120 and 135°C until a clear, molten solution was obtained. If a slurry of another explosive or additive was desired, it was added and mixed until uniform. The mixture was poured and spread onto a thin sheet on Teflon. While cooling, the sheet went through a pliable stage to a brittle stage. The cooled sheet was ground and pressed at 60 to 100°C under vacuum into cylindrical charges.

III. YESTING METHODS

Sensitivity Tests

Mixtures were tested for safety by finding impact and thermal sensitivities. The wedge test gave additional information on initiation.

Impact sensitivity was found on an ERL-type machine equipped with type 12 tools and a microphone for sound analysis. A 40 mg sample heaped on a square of mandpaper was placed under an anvil and a 2.5 kg weight was dropped onto the anvil. No sandpaper is used for type 128. An arbitrary level

of sound indicated a "go." The 50% "go" height was determined by the Bruceton Up and Down method (12).

The thermal sensitivity was measured by the modified Henkin method as developed by Rogers (13) and Janney. A thin slab of explosive was confined in a cartridge, placed in a temperature controlled bath of Wood's metal, and timed until explosion. The temperature below which it will not explode is the critical temperature.

The wedge test, a measure of distance of run of a shock before detonation starts in an explosive, was done at Los Alamos by the Detonation Physics group (14) on 30°-angle mini-wedges machined from 2.54-cm-diam pressed cylinders. Three pressures were used to find the relationship of the run to detonation, X°, to the pressure input.

Performance Tests

The detonation velocity was measured by two groups at Los Alamos. The method used by the Detonation Physics group has been described by Engelke (15); it is very accurate. The Los Alamos Explosives Technology group's method follows.

Ionization switches made of polyamide-insulated, four-mil copper wire were placed about 2.54 mm apart between the charges. The passage of the tonized detonation wave triggered a timer, accurate to • 10 nanoseconds. We used a stack of six 2.54cm-diam charges held tightly in place on a 5.08-cm-thick steel plate with tape. The dent was measured by a ball and ring method. Plate dents of the standard explosives have been correlated by Smith (16) and Urizar. For this 2.54-cm-diam unconfined plate dent test, a factor of 5.68 multiplied by the dent (am) gave the detonation pressure (GPa).

Cylinder tests were done by the Los Alamos Detonation Physics group. The samples were fired in a 2.54-cm-inner-diam by 10.48-cm-long copper tube or a 5.08-cm-inner diam by 60.96-cm-long copper tube. A streak camera recorded the expansion of the copper at a slit 20.32 cm down the tube and appropriately scaled in the 5.08-cm tube. The time versus expansion data were analyzed by fitting a power curve through 10 points aurrounding the 6-, 19-, and 10-mm points of expansion and by finding the first differential for velocity and the second differential for acceleration at

each point (8). Energy of the expansion was compared to TNT by dividing the square of the velocity by the square of the velocity of TNT at the same expansion.

The aquarium test to compare the shock wave in water to what would be calculated was fired at Los Alamos by the Detonation Physics group with calculations done by the Detonation Theory and Application group (17).

The heat of detonation and products were determined in the calorimeter at LLNL as described by Ornelias (18).

IV. RESULTS

Sensitivity

We found that the impact and thermal sensitivities showed AN/ADNT and EDD/AN extection to be moderately insensitive and dafe for most processes. See Table 1 for a comparison of the formulations tested with standard explosives. Note the critical temperature of AN/ADNT with nitroguanidine (NO), which is higher than either AN/ADNT or NO.

The wedge test showed that the shock sensitivity crosses the value of Composition B at a pressure of 6.8 GPa, but incause the slope is different, it will have a longer run at lower shocks and a shorter run at higher shocks it extrapolates to very small runs to detonation at 115 GPa. Table 2 and Figure 1).

Performance

Initial plate dent tests on ANY-ADNT mixtures were done in 1.27-cm-diam recause of the limited supply of ADNT (Table 1). We were surprised that formulation containing almost 50% AN sustained betonation in a 1.27-cm-diam charge that was unconfined and gave a good dent. The pressure derived from dents was compared to that calculated by C. L. Mider of Los Alamos with the BKW hydrodynamics computer code (14). The 1.27-cm size was close to the failure diameter (one failed at high fensity) so subsequent tests were performed on 2.54-cm-diameters.

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TABLE 1 Sensitivity Tests

Material (molar ratios)	Impact Ser Type 12(cm)	nsitivity 12B(cm)	Critical Temperature Heakin (°C)
timo tat Edetos	17Pe 12(Cm)	IZB (Cm)	neakin (°C)
ADNT	58	96	225
ADNT 2H2O	224	> 320	
AN	> 320	>320	361
1.38/1-AN/ADNT	66	71	236
2/1-AN/ADNT	65	65	241
2/1/1.3-AN/ADNT/TATB	250	270	236
1.38/1/1.54-AN/ADNT/RDX	37	70	215
5/1/1-AN/ADNT/RDX	44	7.4	219
5/1/1/3.3-AN/ADNT/RDX/A1	38	55	221
EDD	88	115	245
2.33/1-AN/EDO	109	153	244
3.7/1/1-AN/ADNT/EDD	93	99	212
3/0.3/1-AN/ADNT/EDD	58	96	227
FDEK	74	76	226
1.38/1/1.38-AN/ADNT/NQ	108	210	256
1.38/1/1.83-AN/ADNT/NQ	312	>320	261
NO	`320	-320	198
RD X	22	30	214
TNT	150	- 320	283

where:
AN = ammonium nitrate

AN = ammonium nitrate

ADNT = ammonium dinitrotriazolate

EDD = ethylenediamine dinitrate

NQ = nitroquanidine

RDX = dyclotrimethylene trinitramine

TATB = 1,3,5-triamino-2,4,6-trinitrobenzene

TNT = 1,3,5-trinitrotoluene

Al = aluminum

FDEK = 2.55/0.3/1/0.36 = AN/ADNT/EDD/Potassium Nitrate (KN)

TABLE 2 Wedge Test Data on 2/1 - AN/ADNT

			
7	First Shot	Second Shot	Third Shot
Density (g/cm ³)	1.640	1.640	1.640
Input Pressure (GPa)	6.9	8.7	7.8
Run to Detonation (mm)	6.1	2.7	4.8
Time (us)	1.28	0.35	0. 0

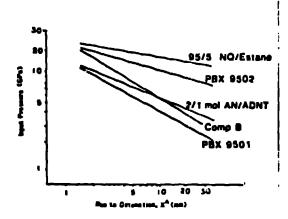
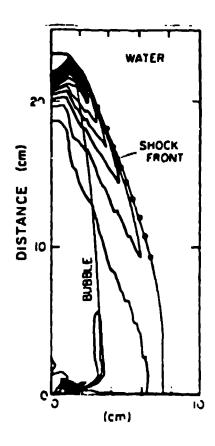


Fig. 1
Relative Shock Sensitivities of 2/1
AN/ADNT and Other Explosives in the W.dee Test.

PBX 9501 - 95/2.5/2.5 wt% HMX/Estane/-NP PBX 9502 - 95/5 wt% TATE/Kel-F 800

Later, plate dent tests were done in conjunction with detonation velocity tests on 2.54-cm-diam charges (Table 4). We found that the addition of extra AN to the eutectic formulation reduced the agreement with the calculated values with the exception of the aluminized 2/1 molar ratio AN/ADNT, which performed better than calculated.

An aquarium test on the 1.38/1/1.5 molar ratio AN/ADNT/RDX showed that the experimental snock in water was the same as the calculated pressure profile (Figure 2).



Admarian test (1), 1-1/1.7-AN ADMT PDX. The lives are the domputer-denotated bruck-wave curves and the counts are the experimental late.

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TABLE]

Material (moler ratio)	Density (g/cm ³)	Extrapolated Per (GPa)	Calculated P.J
2/1-AN/ADNT	1.590	25.2	25.4
	1.645	23.0	27.6
1.38/1-AN/ADNT	1.630	27.3	26.7
	Ϊ,410	Yailed	26,7
1.38/1/1.38-AN/AUNT/NQ	1.654	26.1	28.0
1.38/1/1.5-AN/ADNT/RDX	1.708	33.6	30.4
1.36/1/1-AN/ADNT/HMX	1.756	34.2	32.4

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TABLE 4 Unconfined 2.54-cm Rate Stick/Plate Dent Tests

Material	Density	Experimenta	1	Calcul	ated
(molar ratio)	(g/cm ³)	PcJ(dent) (GPa)	D(m/s)	Pcy(GPa)	D(m/s
2/1-AN/ADNT	1.649	26.1	7892 <u>+</u> 1	27.3	8268
1.38/1/1.5-AN/ADNT/RDX	1.717	31.7	8455 <u>+</u> 2	30.6	8475
5/1/1-AN/ADNT/RDX	1.699	24.0	7712 <u>+</u> 1	30.4	8598
5/1/1/3.3-AN/ADNT/RDX/A1	1.752	25.0	7739 <u>+</u> 10	29.1	8223
2/1/2.66-AN/ADNT/A1	1.734	26.3	7844	25.1	7680
2/1/1.3-AN/ADNT/TATB	1.765	28.3	7845 <u>+</u> 1	28.0	6013
1.38/1/1.38-AN/ADNT/NQ	1.655	26.4		20.0	8305
1.38/1/1.83-AN/ADNT/NQ	1.654	25. 5	3160	26.8	8197
3/1/1-AN/ADNT/EDD	1.607	24.2	7664 <u>+</u> 1	27.4	8287
1/0.3/1-AN/ADNT/EDD	1.535	20.8		23.0	7873

The cylinder tests showed that the ability to push metal of the eutectic explosives was better than TMT (Table 5). These tests showed the effect of diameter on the chavior of intermolecular explosives. Compacison with the EDD/AN 5.08-cm and 10.16-cm cylinder tests showed their similarity in ratformance.

With detonation calorimetry we found that the heat of detonation and the products of 2/1 molar ratio AN:monomolecular compound (Table b) from a BKWR Tiger calculation at freeze-out temperatures of 15000K and 18000K.

TARLE 5 Critmler Tests

	7 1 7.54	A: 4 <u>1</u>	A4 / 1945 (2) 18 / 191	क्षात्रकार अ <u>ग</u> ्रा	A4 - A1 - P A1		156 T	71. 2	
wnesty (4/cm ³)	1.41	1.50	1,418	1. 40	1.411	1,010	1,531		
mt. vol. (m/s)	6.950	.444	-440	* 400	-4:0	1610	1550	"A 70	
Cylinder Well Volumity (SM, 48)				•					
10 =	1.23 1.49 1.44	1.10 1.49 1.33	1,17 1,11 (1,57,6	1.11	1.27 1.44 1.52	1,11	1.10	1.45	1.51
Tylinder Frem Ly Polative to INT of/od THT									
17 = 10 =	1.00 1.00	1.1; 1.11 1.10	1.25 1.17 (1.161)	1.40	1.77	1.1° 1.11 1.11	1.12	1.79 1.77 1.60	1.19

Presention to this point was put filmed. This number was projected by averaging the establish increment of APRT, 180, and the is on FDD/AR cylinders.
2.4 APRT is the 2/1 miler retio of 4°,6/52.6 which return partire
AN/APRT/AL is the 2/1/2,66 maler ratio of 13,2 41,2 17,6 which ratio minime.

EDDIAN IN 178.13 molar ratio or 50 % -- Link ratio minture

TABLE 6
The Detonation Calorimetry Test of 2/1-AN/ADNT

Density was 1.639 g/cm ³ -AH detonation (cal/g) Products (mol/mol HE)		1213±12	126]:40 (from product BKWR CJ Isentrope		
			1520K	1825K	
н³о	1.78		1.77	1.78	
¥ ₂	1.47		1.49	1.49	
co ₂	0.59		0.57	7.59	
112	0.0096		0.0032	0.0025	
co	0,0092		1,0061	0.0065	
40	0.0013		า	1	
ин 3	0.0006		a,59 08	1.010	
нся	0,0005		1)	

V. DISCUSSION

Most explosives containing AN have large critical diameters and even larger ideal diameters. For example, 50/50 AN/TNT (density of 1.53 7/cm³) has a critical diameter of 1.5 cm where D is 4500 m/s and an ideal diameter of 13 cm where D is 6300 m/s. The particle site, the density, and the degree of confinement affect the two diameters (18). Campbell and Engelse (18) reported the slowing of D as the diameter of the explosive approached the critical diameter. The amount of curvature is characteristic of the explosive, influenced by the reaction zone length.

The behavior of entectic AN/ADNT is different because the critical disameter is about 1 cm and the ideal disameter about 2.54 cm. (D of unconfined rate stick and confined cylinder test of 2/1-AN/ADNT are the same; see Teble 3 and 4.) D is about what would be expected from calculation (19) (Table 3).

This small ideal Diameter is not found in every extectic. Again (d) has found that there was considerable difference in D of EDD/AN confined at 2.54-cm-diam. A500 m/s, and at 13.16-cm-diam. The mile are compared the particle size of mach eutectic by scanning electron microscopy and find that the AN particles in EDD/AN have a width of about 10 m whereas the AN particles in AN ADNT eutectic average 1-3 m. As the ratio of AN/ADNT gets further from eutectic formulation, the particle size of AN increases to the same size as the AN in EDD/AN.

Another difference in the properties of the two expectics occurs in the heat if formation. ADNT has a more positive heat of formation, 0.6 a 2 kcalemol, than EDD, -156.1 kcalemol. That gives AN'ADNT more chemical energy to release dirical letonation, 1.10 kcale versus 2.45 kcale for extention EDD AN (water an eas).

Me have not determined which factor is more important or whether

there is some other factor, which is not obvious now, that makes the difference. There are projects in progress to find ways to decrease the particle size of the AN in EDD/AN mixtures and search for other explosives that form eutectics with AN that would have different heats of formation,

Another way to increase the temperature in the detonation zone is to add aluminum metal powder. This should help increase the ideality of the performance because the temperature of the detonation affects the layer thickness of a particle of AN that will react in the detonation zone (19). We see that this is the case when going from the mixture 5/1/1 molar ratio AN/ADNT/RDX to one containing aluminum, 5/1/1/3.1 molar ratio AN/ADNT/RDX/A1. The detonation velocity increased from 90% to 94% of the calculated value. Addition of aluminum to 2/1 molar ratio AN/ADNT increased D from 95% to 102% of the calculated value. We tested the latter composition in the 2.54-cm-diam cylinder test. We found, as did Finger (20) and Bjarnholt (21), that aluminum behaves as an inert in the early part of the expansion (6 mm) but keeps the wall accelerating even at 10 mm. The wall velocity is almost as fast at 19 mm and is faster than the projected value of the 2/1 molar ratio AN/ADNT at 10 mm (Table 4). The pro-jected value was determined by averaging the increments of the other cylinder tests that have D almost as calculated. The tests with D considerably less than calculated showed a higher increase in wall velocity from 19 to 30 mm than those with D close to calculated.

We have discussed ideality as the ability of an intermolecular explonive to follow calculated performance as do the monomolecular explosives that were used to calibrate the calculations. In the BRW calculations the agreement is not too good unless the ratios of the elements making up the new explosive are almost the same as in the model compound, RDX. Many of the intermolecular explosives have a much higher ratio of hydrogen to carbon than does RDX so they probably would not fit the calculation as well. For example, the RDX has C/H/O atom ratio 1/2/2 and 1.38/1 AN/AUNT has C/H/O atom ratio 1/4.76/4.07 but 2.33/1 molar ratio AN/EDD has C/H/O atom ratio 1/9.64/6.48.

Another way to look at ideality is by measuring the detonation products and comparing the result with what would be expected for complete reaction before freeze-out. The detonation calorimetry experiment (Table 6) showed that the products from the detonation of 2/1 molar ratio AN/ADNT, the CO2-balanced intermolecular formulation, were what was expected. oxygen from the AN has been used by the C or CO from the ADNT to form CO2 almost exclusively. The recovery of the products was excellent because there were no solid products. There is definitely complete reaction in this case before freeze-out of the products.

As we study these eutectic systems and find others, we will better understand the parameters that arfect the reactions between molecules in the detonation zone.

ACKNOWLEDGIEMENTS

The author greatly appreciates the contributions in technical nelp and understanding given by Marion L. Clancy, M. L. Clancy, C. E. Hannatori, W. P. Fos, Joan L. Janney, M. J. Urizar, H. H. Cady, M. D. Coburn, Kien Y. Lee, R. P. Engelke, A. W. Campbell, C. W. Mautz, J. B. Ramsey, C. L. Mader, B. G. Craig, and especially the support by R. N. Rogers and conversations with I. B. Akst.

The work was supported in part by the Naval Sea Systems Command and Naval Surface Weapons Center block program under Department of Energy contract W-7405-ENG-36.

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